

10/568802

IAP20 Rec'd PCT/PTO 17 FEB 2006

SUBSTITUTE SPECIFICATION: CLEAN COPY

BACKGROUND OF THE INVENTION

[0001] The present invention relates to a brake system of the 'brake-by-wire' type for actuating a motor vehicle brake system comprising a brake booster which is operable in response to the driver's wish both by means of a brake pedal and by means of an electronic regulating and control unit, with a means being provided to decouple a force-transmitting connection between the brake pedal and the brake booster in the 'brake-by-wire' operating mode, a master brake cylinder connected downstream of the brake booster in terms of effect, to the pressure chambers of which wheel brakes of the motor vehicle are connected, a pedal travel simulator which interacts with the brake pedal and due to which a resetting force acting on the brake pedal can be simulated in the 'brake-by-wire' operating mode independently of an actuation of the brake booster, and which can be enabled in the 'brake-by-wire' operating mode when the force-transmitting connection between the brake pedal and the brake booster is decoupled and can be disabled outside the 'brake-by-wire' operating mode, a first sensor to sense the brake pedal actuating travel, a second sensor to sense the travel of an output member (push rod) of the brake booster, and a third sensor (i.e. a pressure sensor) to sense the brake pressure prevailing in the system, the signals of which sensors are sent to the electronic regulating and control unit.

[0002] A brake system of this type is disclosed in the applicant's international patent application WO 2004/005095. It can be taken from the disclosure of the mentioned patent application that the electronic regulating and control unit initiates appropriate safety procedures, in particular a hydraulic

fallback mode, on account of detected deviations between preset nominal values and actual values measured by means of the sensors. However, no hints can be taken from the document as to how failure of the hydraulic fallback mode being caused e.g. by the inclusion of air or the occurrence of leakages in the system, can be recognized by the driver or detected by the system, respectively.

SUMMARY OF THE INVENTION

[0003] In view of the above, an object of the invention is to disclose measures in a brake system of the type mentioned hereinabove, which render it possible to compensate increased pressure fluid volume absorption in the case of a fault, which is caused by e.g. the inclusion of air or a brake circuit failure, by using control technique means.

[0004] A first solution of this object involves that the electronic regulating and control unit includes a control circuit for controlling the travel covered by the output member of the brake booster, the nominal value thereof being calculated corresponding to the actuating travel of the brake pedal, with a monitoring module being provided which, in the case of a fault such as the inclusion of air or brake circuit failure, performs a partial compensation of the extension of the travel covered by the output member of the brake booster, which extension is caused by the fault.

[0005] A second solution of the object referred to hereinabove involves that the electronic regulating and control unit includes a control circuit for controlling the travel covered by the output member of the brake booster and the hydraulic pressure prevailing in the system, the nominal values thereof being calculated corresponding to the actuating travel of the brake pedal, with a

monitoring module being provided which, in the case of a fault such as the inclusion of air or brake circuit failure, switches the control circuit from the travel control mode to the pressure control mode in order to perform a compensation of the extension of the travel covered by the output member of the brake booster, which extension is caused by the fault.

[0006] In a favorable improvement of the first solution of the invention, the partial compensation of the extension of the travel covered by the output member of the brake booster, which extension is caused by the fault, is performed by adding a correction value to the nominal value.

[0007] In another favorable embodiment of the subject matter of the invention, a pressure fluid volume/pressure characteristic curve is stored in the monitoring module, i.e. the dependency of the pressure fluid volume absorption of the brakes or of the travel covered by the output member of the brake booster and corresponding to the pressure fluid volume absorption on the hydraulic pressure (p) Q or $S_{Ds} = f(p)$, and the monitoring module is furnished with the actual values of the travel covered by the output member of the brake booster and of the hydraulic pressure prevailing in the system, and a travel value corresponding to the nominal value of the pressure fluid volume is calculated from the actual pressure value and compared with the actual value of the travel covered by the output member of the brake booster, and a fault in the system is concluded when the comparison result exceeds a threshold value.

[0008] The above-mentioned correction value can preferably correspond to half the result of the comparison.

[0009] In another advantageous improvement of the subject matter of the invention, the control quality is considerably enhanced in that the actual values undergo a low-pass filtering operation.

[0010] In another favorable feature of the invention, a transition function, e.g. low-pass filtering or a ramp function, is activated when a case of fault is detected.

[0011] It is furthermore provided according to another feature of the invention that a warning lamp is activated when a case of fault is detected in the system.

BRIEF DESCRIPTION OF THE DRAWINGS

[0012] Further features and advantages of the invention will be explained in detail in the following description by way of two embodiments, making reference to the accompanying drawings. In the drawings:

[0013] Figure 1 is a schematic view of the brake system of the invention;

[0014] Figure 2 shows a block diagram of a first design of a control circuit of the invention;

[0015] Figure 3 shows a block diagram of a second design of a control circuit of the invention; and

[0016] Figure 4 shows a diagram view of the mode of operation of the second design of the control circuit shown in Figure 3.

DETAILED DESCRIPTION OF THE DRAWINGS

[0017] The brake system shown in a schematic view in Figure 1 and intended for the actuation of a motor vehicle brake system of the 'brake-by-wire' type essentially comprises a brake booster, preferably a vacuum brake booster 3, a master brake cylinder connected downstream of the brake booster 3, preferably a tandem master cylinder 4, to the pressure chambers (not shown) of which wheel brakes 13, 14, 15, 16 of a motor vehicle are connected by the intermediary of a hydraulic control unit 17, a pressure fluid tank 5 associated with the master brake cylinder 4, a brake pedal 1 for actuation of the brake booster 3 by the driver, a pedal travel simulator 2 which cooperates with the brake pedal 1, in particular in the 'brake-by-wire' operating mode and imparts the customary brake pedal feel to the driver, at least one sensor device 6 for sensing a driver's deceleration request or the actuating travel S_{Bp} of the brake pedal 1, as well as an electronic control unit 7, the output signals of which enable, among others, actuation of an electromagnet 8 that is associated with the brake booster 3 and renders it possible to actuate a pneumatic control valve 9 independently of the driver's wish, the said control valve controlling the supply of air to the brake booster 3. As will be explained in detail in the subsequent description, the electronic regulating unit 18 comprises a control circuit for controlling a characteristic quantity of the brake booster 3, preferably the travel S_{Ds} covered by the output member 20 of the brake booster 3, or for controlling the mentioned quantity and the hydraulic pressure prevailing in the system.

[0018] An axial slot 'a' provided between the end of a piston rod 10 coupled to the brake pedal 1 and a control piston 11 of the above-mentioned control valve 9 ensures decoupling the force-transmitting connection between the brake pedal 1 and the brake booster 3 in the 'brake-by-wire' operating mode. A travel sensor

18 is used to sense the travel of a movable wall 19 that generates the boosting force of the brake booster 3 or, respectively, the travel (S_{Ds}) of an output member 20 of the brake booster 3 which transmits its output force onto a non-illustrated first piston of the master brake cylinder 4. Besides, a pressure sensor 21 is integrated into the hydraulic control unit 17 and senses the hydraulic pressure (p) prevailing in the system.

[0019] The pedal travel simulator 2 by which, as has been mentioned above, a resetting force acting on the brake pedal in the 'brake-by-wire' operating mode can be simulated irrespective of an actuation of the brake booster 3 is designed in such a fashion that it can be enabled in the 'brake-by-wire' operating mode when the force-transmitting connection between the brake pedal 1 and the brake booster 3 is decoupled, and can be disabled outside the 'brake-by-wire' operating mode. The pedal travel simulator 2 is actuated by means of an actuating member 12 articulated at the brake pedal 1.

[0020] The first design of the above-mentioned control circuit for controlling the travel S_{Ds} covered by the output member 20 of the brake booster 3 is illustrated in Figure 2 and basically comprises a nominal-value generating module 22, a travel controller 23, and a monitoring module 24. In the nominal-value generating module 22, the nominal value $S_{Dsnominal}$ of travel S_{Ds} covered by the output member 20 of the brake booster 3 is calculated from the actuating travel S_{Bp} of the brake pedal 1 detected by means of the travel sensor 6. The nominal value $S_{Dsnominal}$ to which a correction value S_{corr} calculated in the monitoring module 24 is added in an adder 25, is compared with the actual value $S_{Dsactual}$ of the travel covered by the output member 20 of the brake booster 3, which actual value is detected by means of

the travel sensor 18, whereupon the deviation ΔS calculated this way is sent to the travel controller 23 whose output quantity, an electric voltage U , drives the electromagnet 8. The monitoring module 24, in which a pressure fluid volume/pressure characteristic curve is stored, i.e. the dependency of the pressure fluid volume absorption of the brakes 13 to 16 or of the travel S_{Ds} covered by the output member (20) of the brake booster 3 and corresponding to the pressure fluid volume absorption on the hydraulic pressure (p) Q or $S_{Ds} = f(p)$, is provided as input quantities with the actual values $S_{Dsactual}$, p_{actual} of the travel covered by the output member 20 of the brake booster 3 and of the hydraulic pressure prevailing in the system, which preferably undergo a low-pass filtering operation in associated low-pass filters 26, 27. A travel value S_{model} corresponding to a nominal value of the pressure fluid volume is calculated from the actual pressure value p_{actual} in the monitoring module 24 and compared with the actual value $S_{Dsactual}$ of the travel covered by the output member 20 of the brake booster 3. When the comparison result $\Delta S_{diff} = S_{model} - S_{Dsactual}$ exceeds a threshold value $S_{threshold}$, the above-mentioned correction value S_{corr} is generated which e.g. corresponds to half the value $\Delta S/2$ of the deviation ΔS sent to the travel controller 23. An optical warning, for example, by a warning lamp 31 lighting up, can be produced simultaneously. Addition of the correction value S_{corr} achieves a partial compensation of the extension of the travel $S_{Dsactual}$ covered by the output member 20 of the brake booster 3, which extension is e.g. caused by gas inclusions in the system or a brake circuit failure.

[0021] In the second design of the control circuit illustrated in Figure 3, a nominal-pressure-value generating module 28 is provided in addition to the nominal-travel-value generating module 22 mentioned with respect to Figure 2, in which the nominal value

p_{nominal} of the hydraulic pressure prevailing in the system is calculated from the actuating travel S_{Bp} of the brake pedal 1 that is detected by means of the travel sensor 6. While the nominal travel value $S_{Ds\text{nominal}}$, like in the first design, is compared with the actual travel value $S_{Ds\text{actual}}$ in order to produce the deviation ΔS , a second deviation Δp is produced in a second adder 29 from the nominal pressure value p_{nominal} and the actual pressure value p_{actual} . The two deviations ΔS , Δp are sent to a switch-over device 30 which, in response to the signal $S_{\text{corr}} > 0$ (switch-over condition), switches over from the travel control mode as a standard mode of operation to a pressure control mode. As this occurs, the controller 23 arranges for different parameters for the travel control and the pressure control.

[0022] In order to prevent an abrupt change of the controlled variable in the second design of the control circuit, a transition function, e.g. low-pass filtering or a ramp function, is activated at the time t_1 (point A of the characteristic curve - end of the travel control) of the switch-over operation. This procedure is illustrated in Figure 4, and the characteristic curve $p = f(t)$ characterized by I corresponds to the travel control mode, while the characteristic curve designated by II corresponds to the pressure control mode, and portion A - B corresponds to the transition function. It becomes apparent from the illustration that starting with the time t_2 (point B of the characteristic curve) the control follows the pressure control characteristic curve. The vertical shift L between the two characteristic curves I and II is caused by gas inclusions or leakages, for example.